

Towards 2D overland flow simulations

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Problem context



Preventing overland flow and erosion

From upstream...



(Photos : Yves Le Bissonnais, INRA)

...to downstream.



Downstream zones modifications (watersheds)



- ▶ Where is the water coming from ?
- ▶ Where is it flowing ?

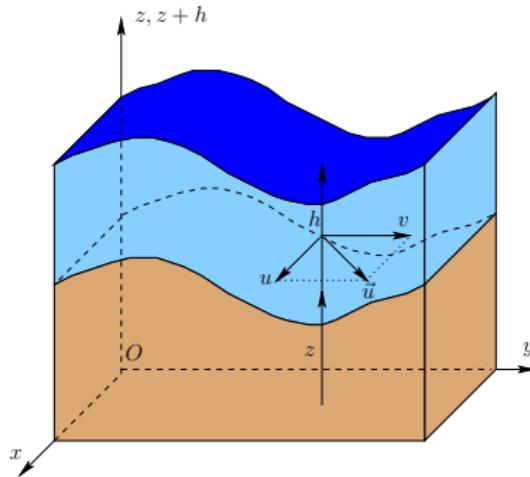
Use of physical models is required to :

- ▶ simulate flow (volumes and location)
- ▶ suggest changes (grass strip).

~~~ to carry out improvements

# Shallow Water (Saint-Venant) system

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Data : topography  $z$ , rain  $P$ , infiltration  $I$

Unknowns : velocities  $u, v$ , water height  $h$

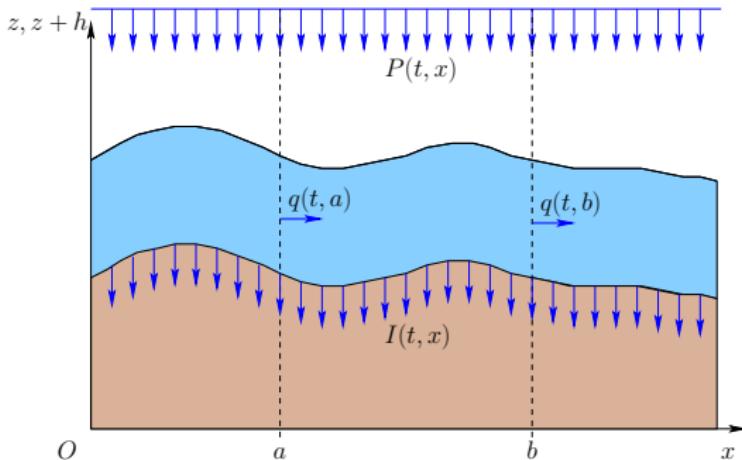
$$\begin{cases} \partial_t h + \partial_x (hu) + \partial_y (hv) = P - I \\ \partial_t (hu) + \partial_x (hu^2 + gh^2/2) + \partial_y (huv) = gh(-\partial_x z - S_{fx}) \\ \partial_t (hv) + \partial_x (huv) + \partial_y (hv^2 + gh^2/2) = gh(-\partial_y z - S_{fy}) \end{cases}$$

## Strategy

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- ▶ Properties of the 1D Shallow Water system
- ▶ Choice of the method depending on the properties
- ▶ Validation : analytical solutions and laboratory experiment
- ▶ Application : field data

# 1D Shallow Water system



Data : topography  $z$ , rain  $P$ , infiltration  $I$

Unknowns : velocities  $u$ , water height  $h$

A system of conservation laws

$$\begin{cases} \partial_t h + \partial_x(hu) = P - I \\ \partial_t(hu) + \partial_x(hu^2 + gh^2/2) = gh(-\partial_x z - S_f) \end{cases} \quad (1)$$

# System properties (I) : Hyperbolicity

Setting  $q = hu$

$$\textcolor{red}{U} = \begin{pmatrix} \textcolor{red}{h} \\ q \end{pmatrix}, F(\textcolor{red}{U}) = \begin{pmatrix} \textcolor{red}{q} \\ \textcolor{red}{q}^2/\textcolor{red}{h} + gh^2/2 \end{pmatrix}, \textcolor{blue}{B} = \begin{pmatrix} \textcolor{blue}{P} - \textcolor{red}{I} \\ g\textcolor{red}{h}(-\partial_x z - S_f) \end{pmatrix},$$

compact form

$$\partial_t \textcolor{red}{U} + \partial_x F(\textcolor{red}{U}) = \partial_t \textcolor{red}{U} + F'(\textcolor{red}{U}) \partial_x \textcolor{red}{U} = \textcolor{blue}{B},$$

Hyperbolicity if  $\textcolor{red}{h} > 0$  :

$$\lambda_-(\textcolor{red}{U}) = \textcolor{red}{u} - \sqrt{gh}, \quad \lambda_+(\textcolor{red}{U}) = \textcolor{red}{u} + \sqrt{gh}$$

| Saint-Venant                                                                                       | gaz dynamic                                                                                    |
|----------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------|
| Froude number $Fr = \frac{ \textcolor{red}{u} }{c}$<br>$c = \sqrt{gh}$ free surface waves celerity | Mach number $\frac{ \textcolor{red}{u} }{c}$<br>$c = \sqrt{p'(\rho)}$ sound speed <sup>1</sup> |
| <u>subcritical</u> $Fr < 1$                                                                        | subsonic                                                                                       |
| <u>supercritical</u> $Fr > 1$                                                                      | supersonic                                                                                     |

1.  $p(\rho) = \rho RT$  perfect gaz

## System properties (II) : Conservation laws

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Integral of equation (1) in  $x$

$$\partial_t \mathbf{h} + \partial_x \mathbf{q} = \mathbf{P} - \mathbf{I},$$

gives

$$\frac{d}{dt} \int_a^b \mathbf{h}(t, x) dx = \mathbf{q}(t, a) - \mathbf{q}(t, b) + \int_a^b \mathbf{P}(t, x) - \mathbf{I}(t, x) dx,$$

Mass **conservation** of water.

Second equation : momentum equation

## System properties (III) : Steady states

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## System properties (III) : **Steady state**

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$$\begin{cases} \partial_t h + \partial_x(hu) = P - I \\ \partial_t(hu) + \partial_x(hu^2 + gh^2/2) = gh(-\partial_x z - S_f) \end{cases} \quad (2)$$

$$\partial_t h = \partial_t u = \partial_t q = 0$$

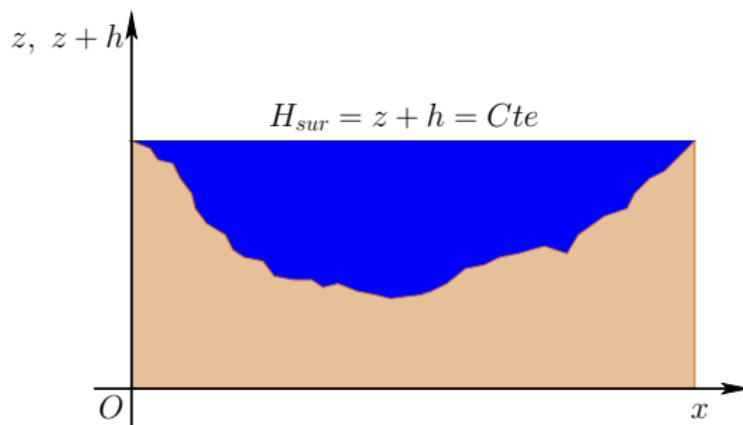
$$\begin{cases} \partial_x hu = P - I \\ \partial_x(hu^2 + gh^2/2) = gh(-\partial_x z - S_f) \end{cases} .$$

## System properties (III) : Steady states

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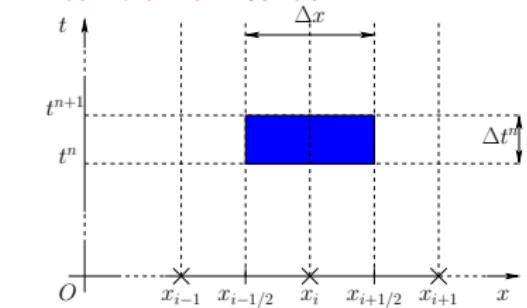
Lac at rest equilibrium

$$\begin{cases} u = 0 \\ g(\textcolor{red}{h+z}) = Cst \end{cases} .$$



# Numerical method (I)

Finite volume method



we get

$$U_i^{n+1} = U_i^n - \frac{\Delta t}{\Delta x} [F_{i+1/2}^n - F_{i-1/2}^n],$$

with the interface flux approximation

$$F_{i+1/2}^n = \mathcal{F}(U_i^n, U_{i+1}^n) \sim \frac{1}{\Delta t} \int_{t^n}^{t^{n+1}} F(U(t, x_{i+1/2})) dt.$$

We integrate  
 $\partial_t \mathbf{U} + \partial_x F(\mathbf{U}) = 0$   
on the volume

[ $t^n, t^{n+1}$ ]  $x_{i-1/2}, x_{i+1/2}$ ,  
and we set  
 $U_i^n = \frac{1}{\Delta x} \int_{x_{i-1/2}}^{x_{i+1/2}} U(t^n, x) dx$

## Numerical method (I)

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- ▶ For each choice of  $\mathcal{F}(U_G, U_D)$  we have a different **finite volume scheme** :  
HLL, kinetic, Rusanov, VF Roe-ncv, suliciu, ...
- ▶ second Order
  - ▶ in space : MUSCL, ENO, modified ENO
  - ▶ in time : Heun

## Numerical method (I)

---

- ▶ For each choice of  $\mathcal{F}(U_G, U_D)$  we have a different **finite volume scheme** :  
HLL, kinetic, Rusanov, VF Roe-ncv, suliciu, ...
- ▶ second Order
  - ▶ in space : MUSCL, ENO, modified ENO
  - ▶ in time : Heun
- ▶ Coupling with the source term (topography  $\partial_x \mathbf{z}$ )  
Necessity : compatibility with steady states

## Steady states (II)

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$$\begin{cases} \partial_t h + \partial_x(hu) = 0 \\ \partial_t(hu) + \partial_x(hu^2 + gh^2/2) = -gh\partial_x z \end{cases} \quad (3)$$

$$\partial_t h = \partial_t u = \partial_t q = 0$$

$$\begin{cases} hu = Cst \\ u^2/2 + g(h+z) = Cst \end{cases} .$$

We consider

$$\begin{cases} u = Cst \\ g(\textcolor{red}{h+z}) = Cst \end{cases} .$$

## Hydrostatic reconstruction (II) [Audusse et al., 2004]

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We define

$$z^* = \max(z_G, z_D)$$

and

$$\begin{cases} U_G^* = (h_G^*, h_G^* u_G), \quad U_D^* = (h_D^*, h_D^* u_D) \\ h_G^* = \max(\textcolor{red}{h_G + z_G - z^*}, 0) \\ h_D^* = \max(\textcolor{red}{h_D + z_D - z^*}, 0) \end{cases} .$$

Thus, we have

$$\begin{cases} \mathcal{F}_G(U_G, U_D, \Delta Z) = \mathcal{F}(U_G^*, U_D^*) + \begin{pmatrix} 0 \\ g(h_G^2 - (h_G^*)^2)/2 \end{pmatrix} \\ \mathcal{F}_D(U_G, U_D, \Delta Z) = \mathcal{F}(U_G^*, U_D^*) + \begin{pmatrix} 0 \\ g(h_D^2 - (h_D^*)^2)/2 \end{pmatrix} \end{cases} ,$$

where  $\mathcal{F}(U_G, U_D)$  is the numerical flux.

## Friction treatment

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Shallow Water system with friction  $f$

$$\begin{cases} \partial_t h + \partial_x(hu) = 0, \\ \partial_t(hu) + \partial_x(hu^2 + gh^2/2) + h\partial_x z = -hf, \end{cases} \quad (4)$$

$f = f(h, u)$  friction force (on the bottom)

Several friction laws possible

- ▶ Manning :  $f = n^2 \frac{u|u|}{h^{4/3}}$
- ▶ Darcy-Weisbach :  $f = F \frac{u|u|}{8gh}$

## Friction treatment

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- ▶ Apparent topography [Bouchut, 2004]

We consider :  $z_{app} = z + b^n$

with  $\partial_x b^n = S_f^n$

# Friction treatment

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- ▶ Apparent topography [Bouchut, 2004]

We consider :  $z_{app} = z + b^n$

with  $\partial_x b^n = S_f^n$

- ▶ Semi-implicit [Bristeau and Coussin, 2001]

$$q_i^{n+1} + F \frac{|q_i^n| q_i^{n+1}}{8h_i^n h_i^{n+1}} \Delta t = q_i^n + \frac{\Delta t}{\Delta x} (F_{i+1/2} - F_{i-1/2})$$

with  $q_i^{n+1*}$  for the right part, we have

$$q_i^{n+1} = \frac{q_i^{n+1*}}{1 + \Delta t \frac{F|u_i^n|}{8h_i^{n+1}}}$$

## Validation on analytical solutions – SWASHES

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New test cases :

- ▶ Saint-Venant/shallow water :
  - ▶ data  $z$
  - ▶ unknowns  $h$  et  $u$  (and so  $q$ )

## Validation on analytical solutions – SWASHES

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New test cases :

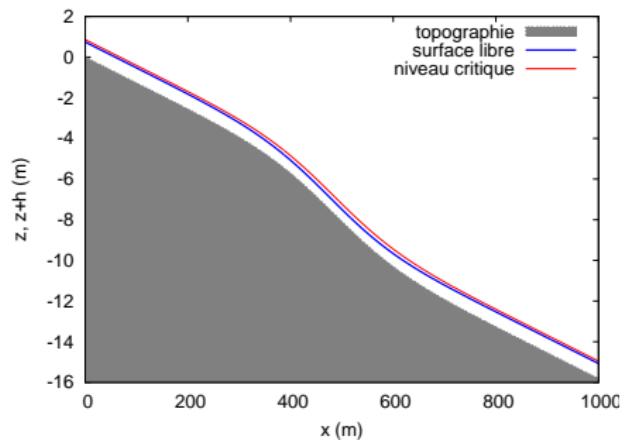
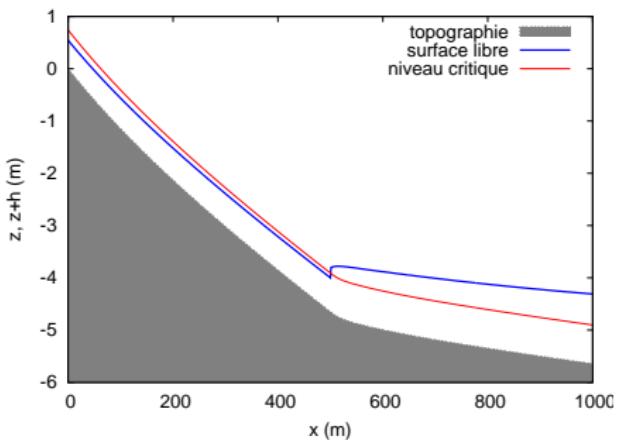
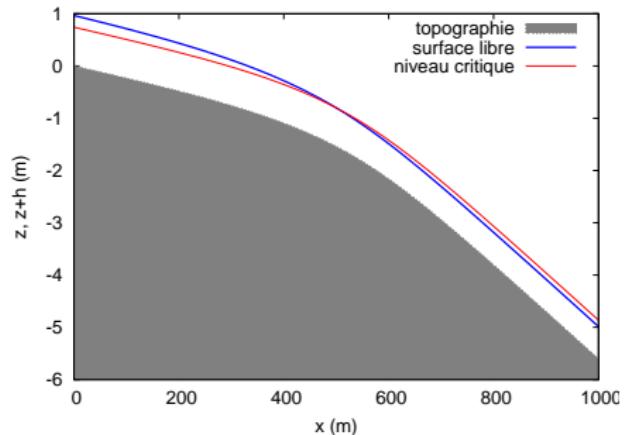
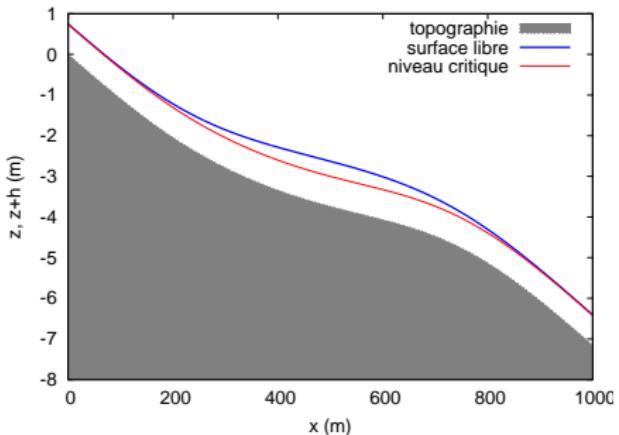
- ▶ Saint-Venant/shallow water :
  - ▶ data  $z$
  - ▶ unknowns  $h$  et  $u$  (and so  $q$ )
- ▶ test cases
  - ▶ data  $h$  and  $q$  (and so  $u$ )
  - ▶ unknown  $z$

## Validation on analytical solutions – SWASHES

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New test cases :

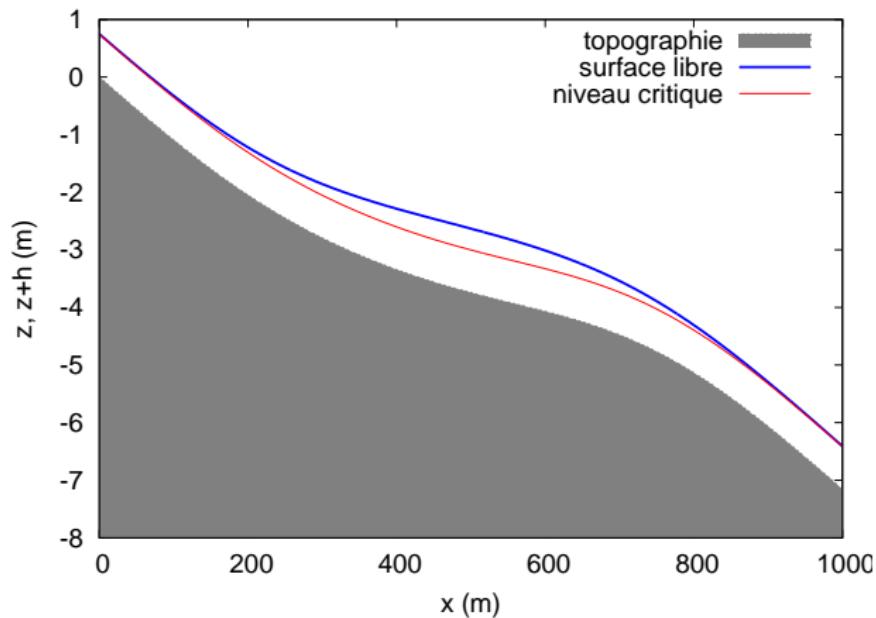
- ▶ Saint-Venant/shallow water :
  - ▶ data  $z$
  - ▶ unknowns  $h$  et  $u$  (and so  $q$ )
- ▶ test cases
  - ▶ data  $h$  and  $q$  (and so  $u$ )
  - ▶ unknown  $z$
- ▶ Several possibilities
  - ▶ several friction laws
  - ▶ diffusion source term [Delestre and Marche, 2010]
  - ▶ rain source term



# Validation on analytical solutions – SWASHES

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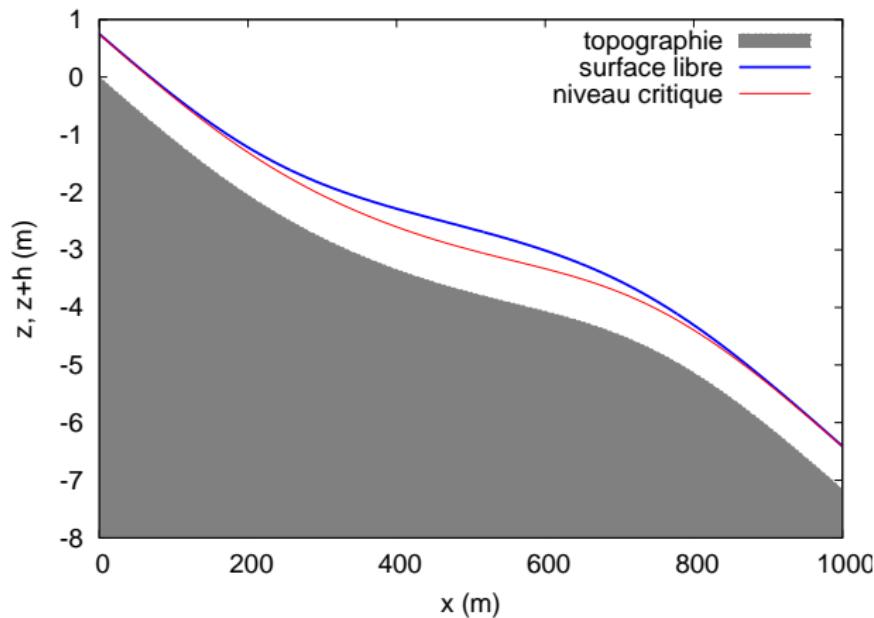
Apparent topography (subcritical-subcritical)



# Validation on analytical solutions – SWASHES

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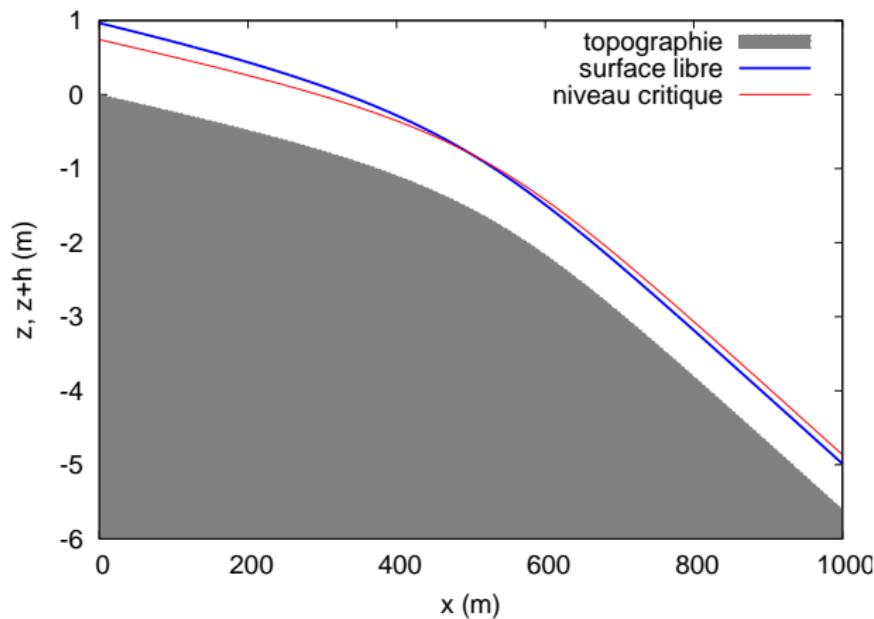
Semi-implicit (subcritical-subcritical)



# Validation on analytical solutions – SWASHES

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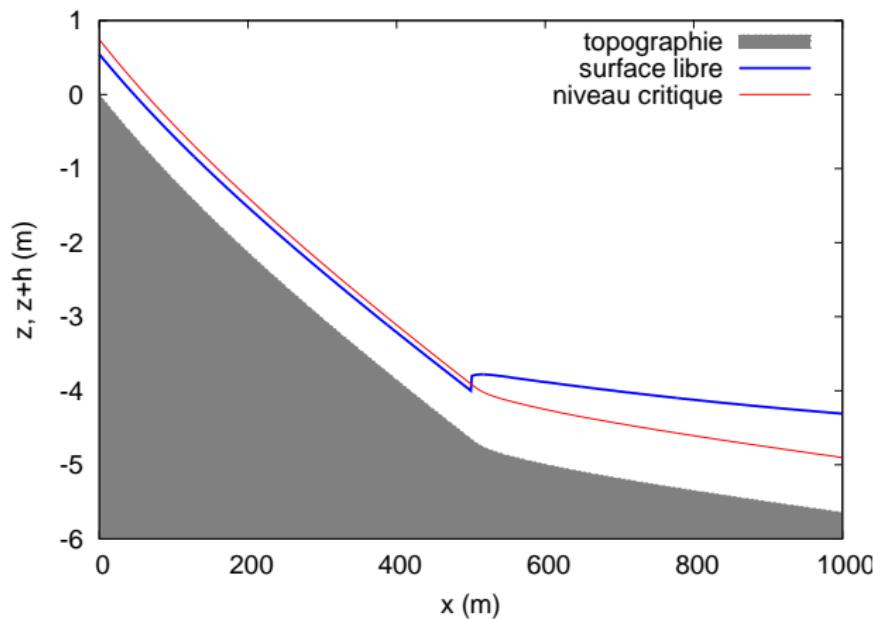
Semi-implicit (subcritical-supercritical)



# Validation on analytical solutions – SWASHES

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Semi-implicit (supercritical-subcritical)



## Summary of the chosen numerical method

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- ▶ Numerical flux : HLL
- ▶ Second order scheme : MUSCL
- ▶ Friction : semi-implicit treatment
- ▶ Shallow Water system with rain  $P$

$$\begin{cases} \partial_t h + \partial_x(hu) = P \\ \partial_t(hu) + \partial_x(hu^2 + gh^2/2) + h\partial_x z = -hf \end{cases} \quad (5)$$

time splitting/explicit treatment

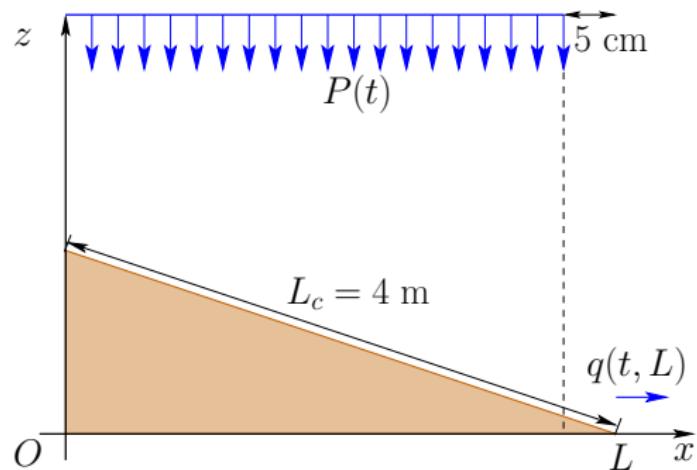
# Validation on experiments – INRA rain simulator

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## Settings of the experiment

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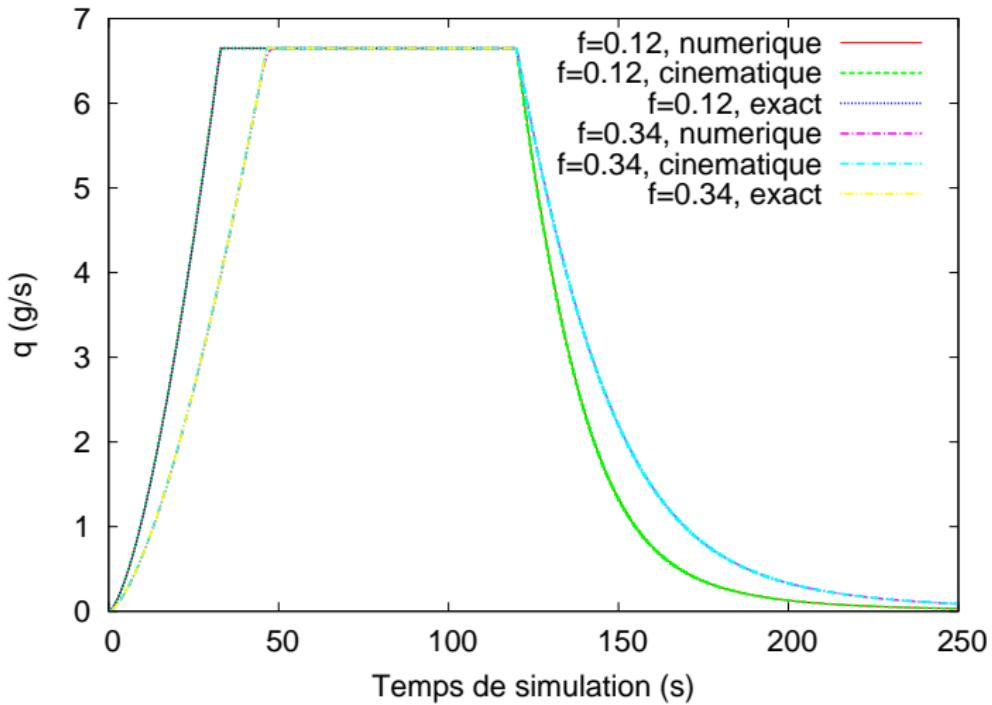


$$0 \leq t \leq 250\text{s}$$

$$R(x, t) = \begin{cases} 50 \text{ mm/h} & \text{if } (x, t) \in [0, L] \times [5, 125] \\ 0 & \text{else} \end{cases}$$

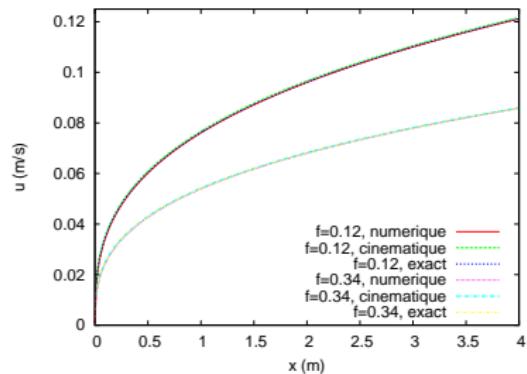
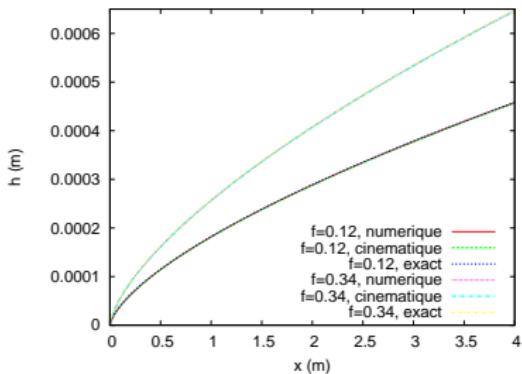
# Analytical solutions and simulations

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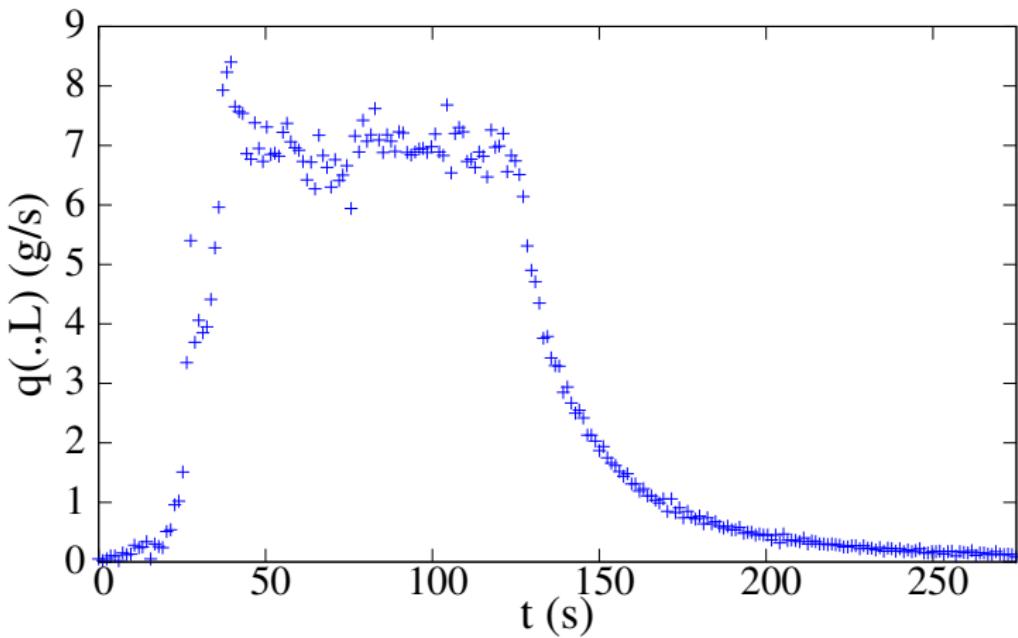
# Water height and velocity at equilibrium

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## What about reality?

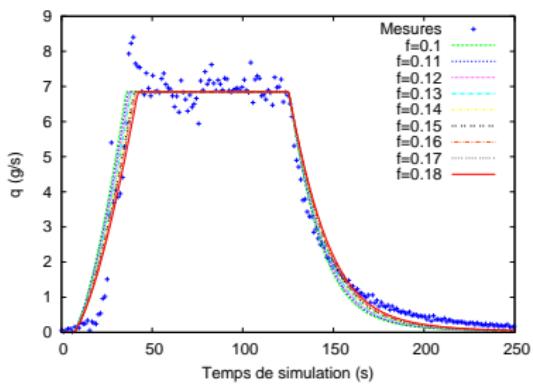
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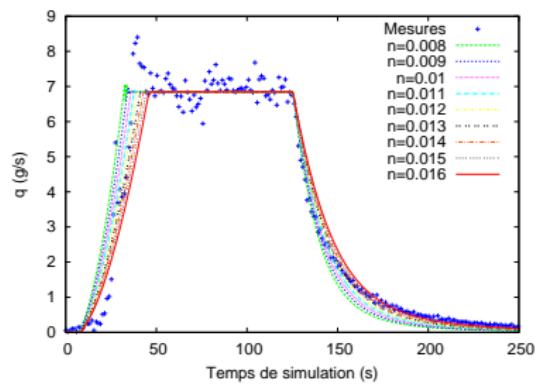
# "Calibration"

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Darcy-Weisbach

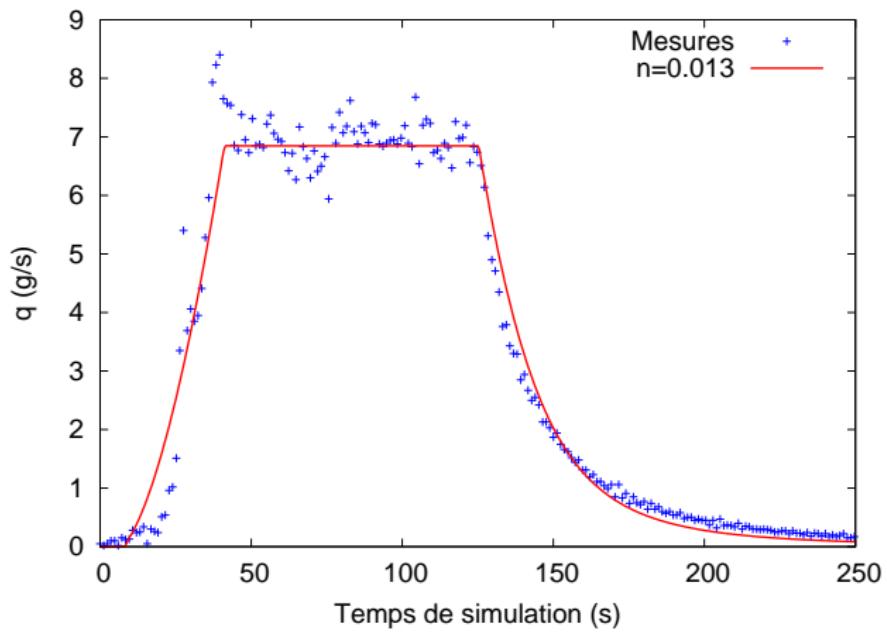


Manning



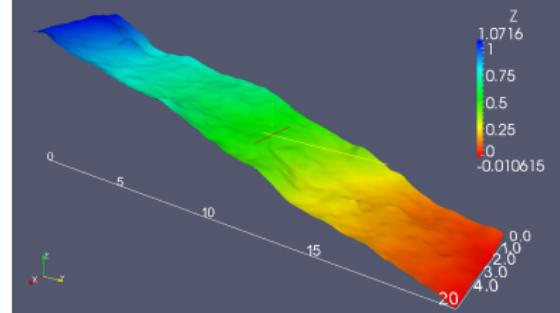
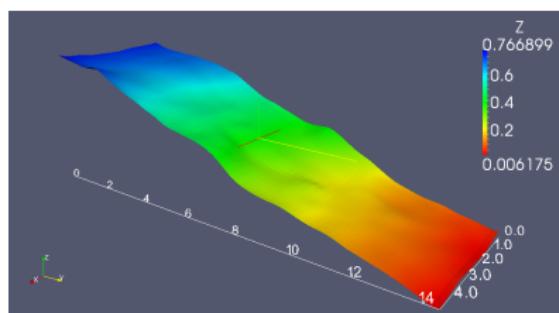
# A simulation result (Manning)

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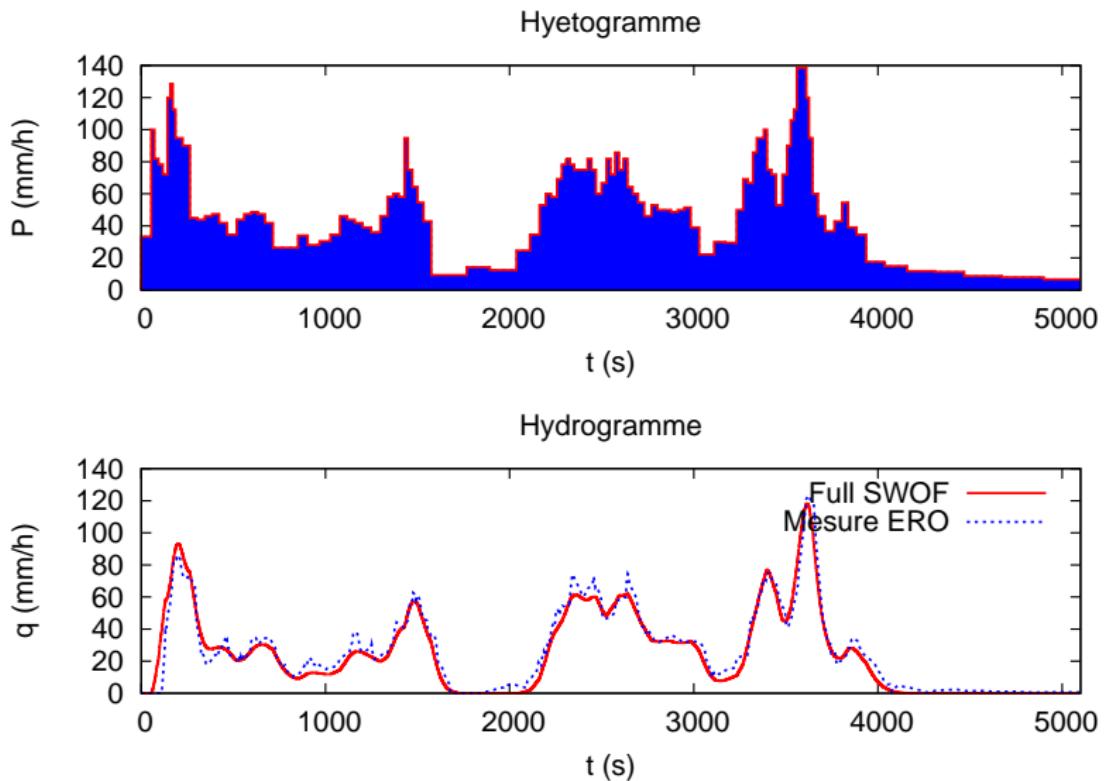
# Parcels in Niger ([Esteves et al., 2000], IRD)

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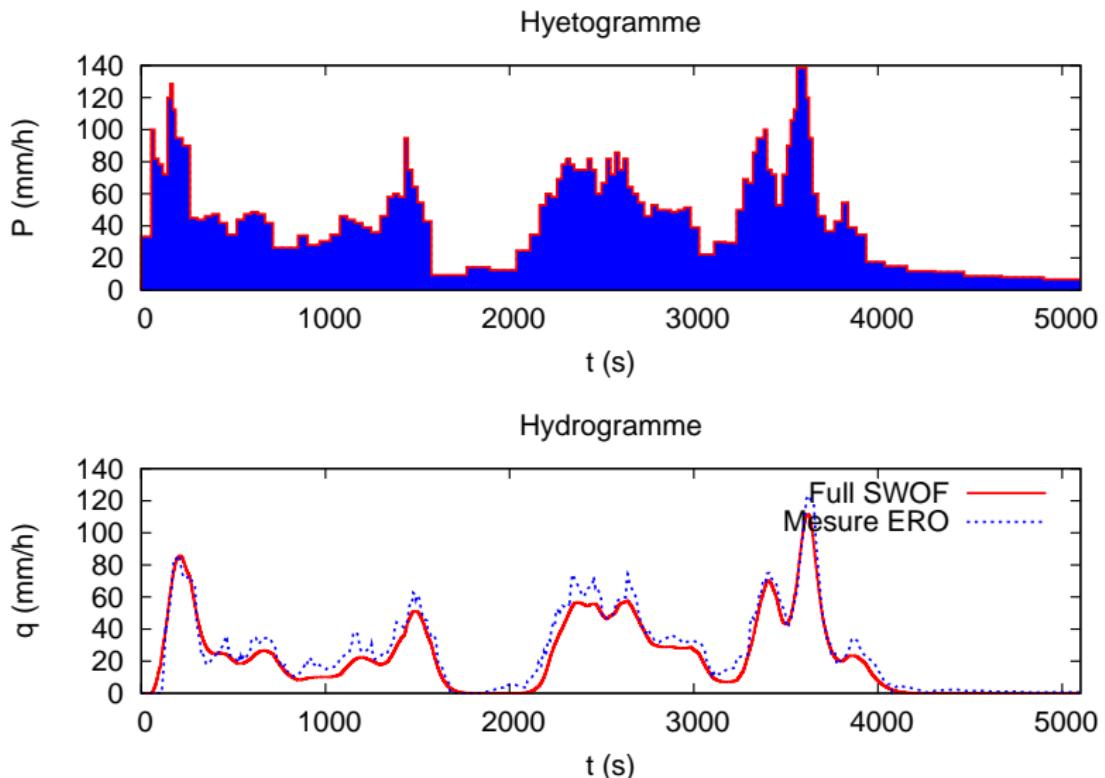
# Darcy-Weisbach

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# Manning

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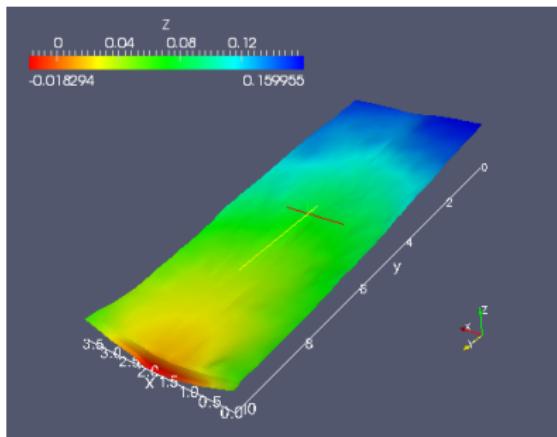


## Thies parcel – Senegal ([Tatard et al., 2008], IRD)

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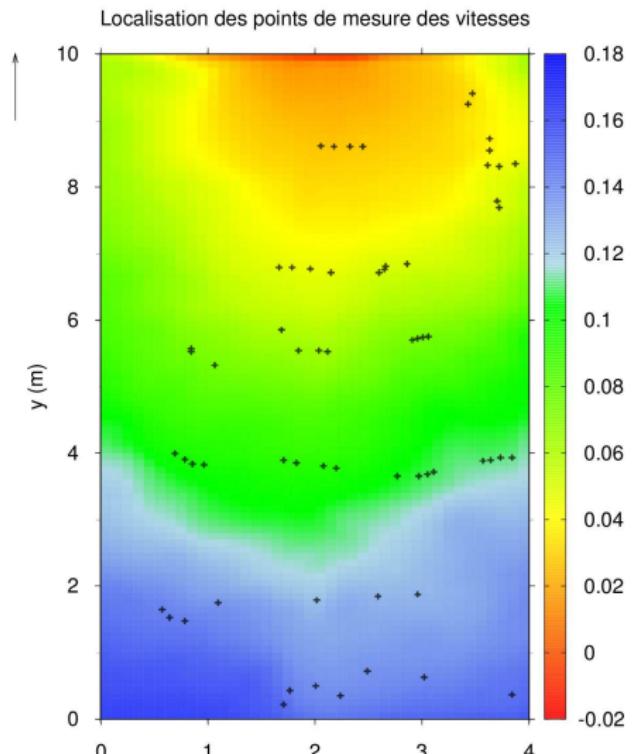
Velocity measures by SVG [Planchon et al., 2005]

Number of cells :  $40 \times 100$  ( $4\text{ m} \times 10\text{ m}$ )



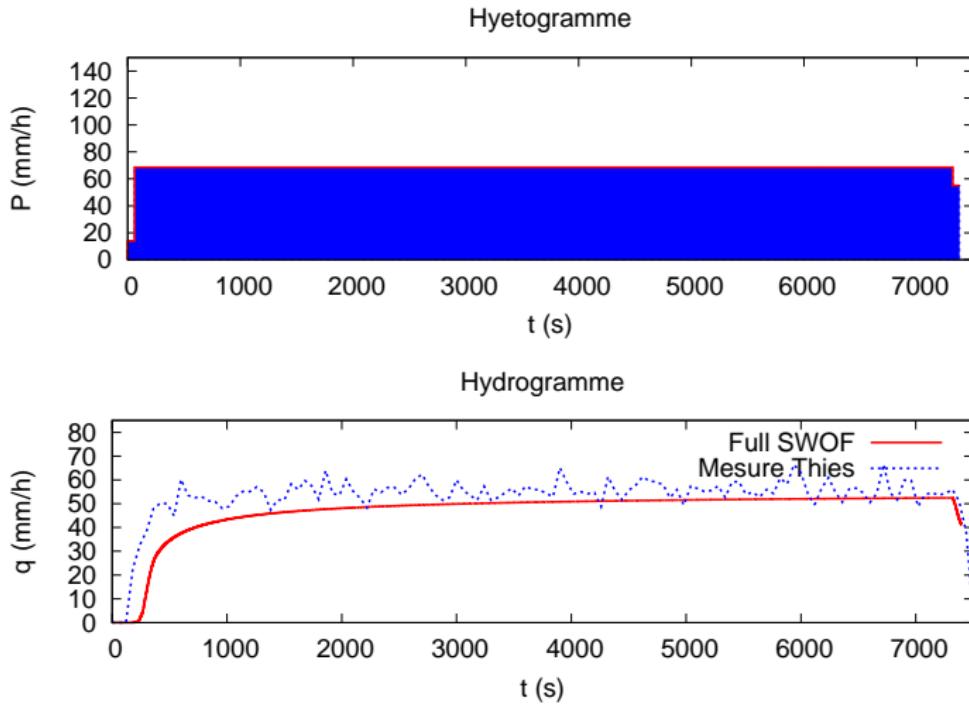
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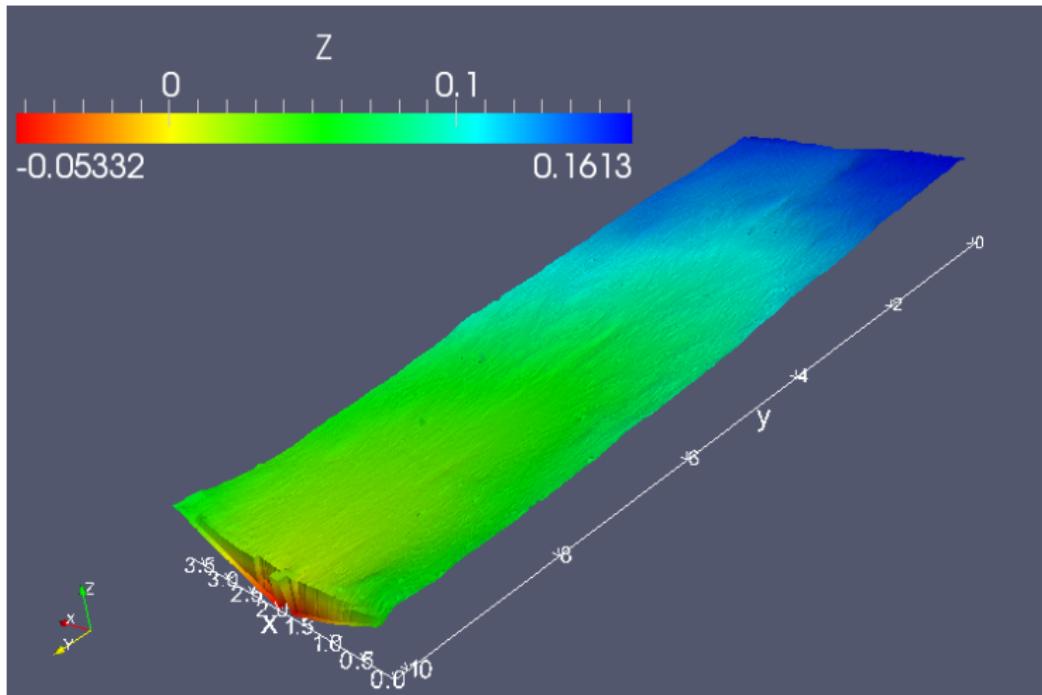
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# Thies parcel – Senegal ([Tatard et al., 2008], IRD)

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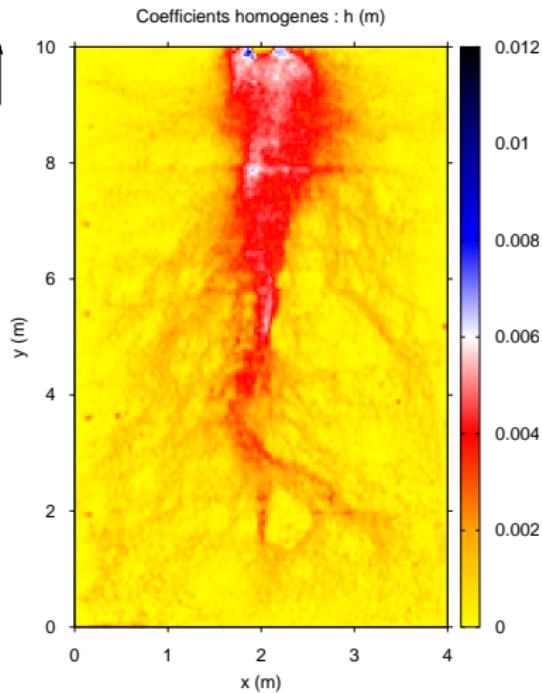
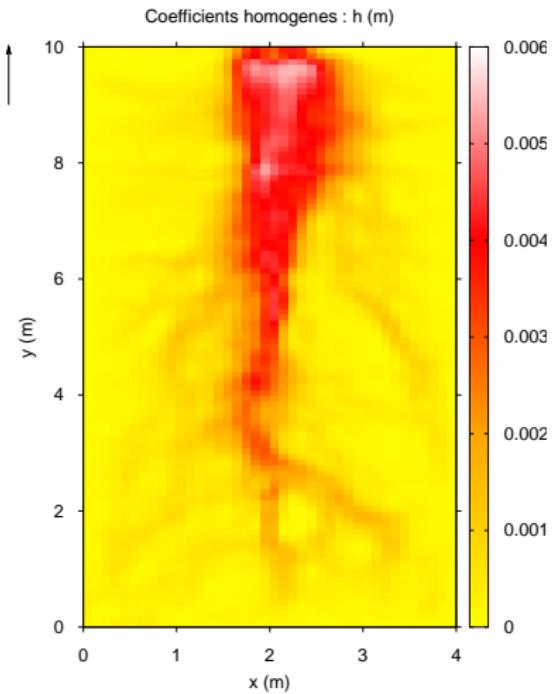
Number of cells :  $160 \times 200$



# Thies parcel – Senegal ([Tatard et al., 2008], IRD)

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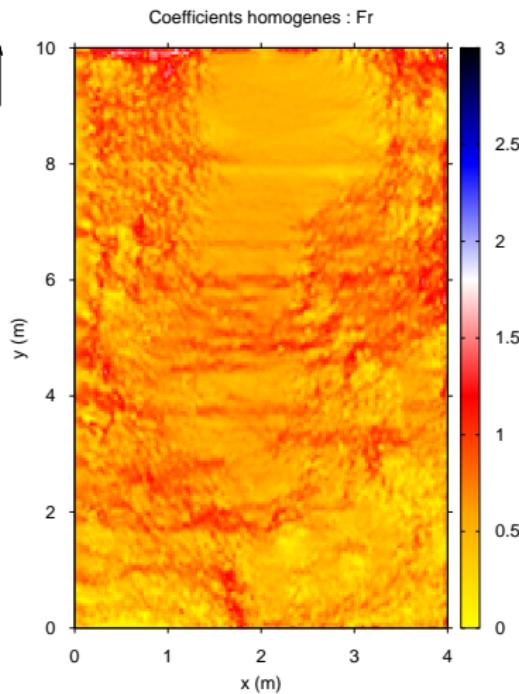
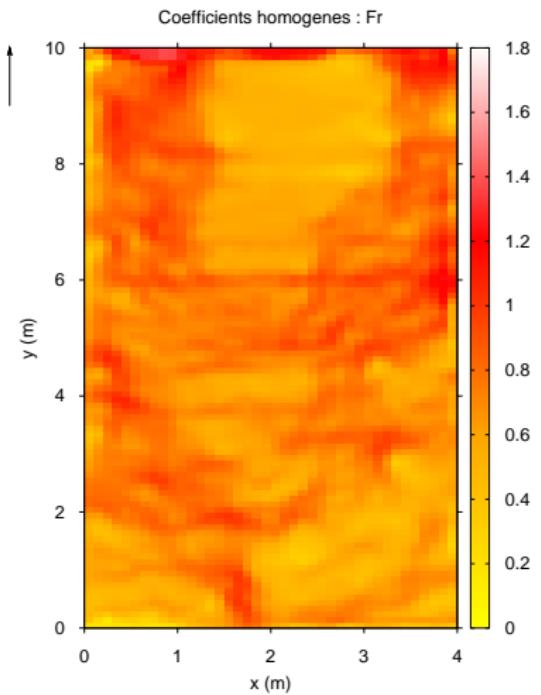
## Homogeneous coefficients



# Thies parcel – Senegal ([Tatard et al., 2008], IRD)

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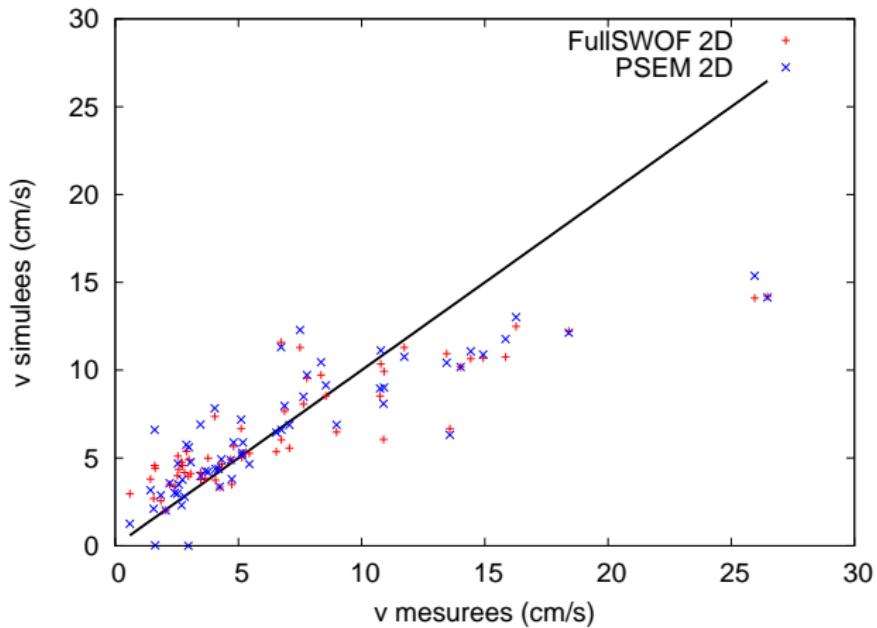
## Homogeneous coefficients



# Thies parcel – Senegal ([Tatard et al., 2008], IRD)

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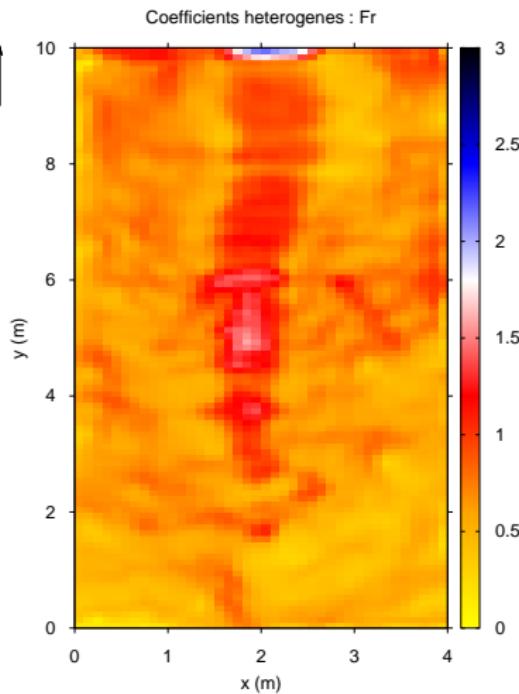
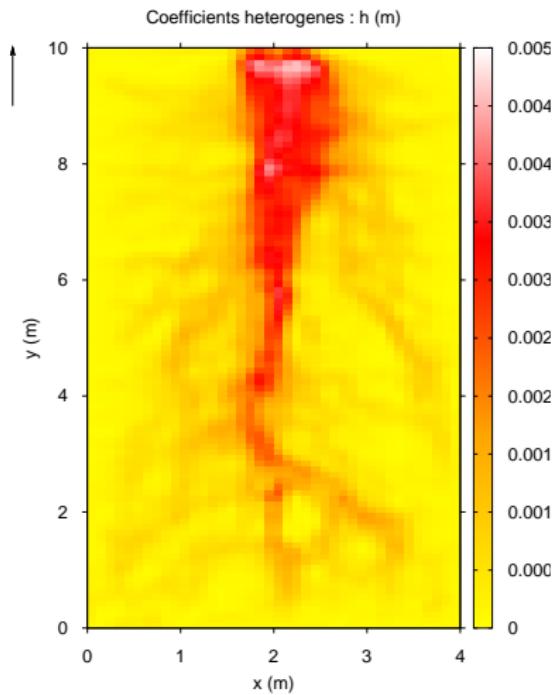
## Velocities



# Thies parcel – Senegal ([Tatard et al., 2008], IRD)

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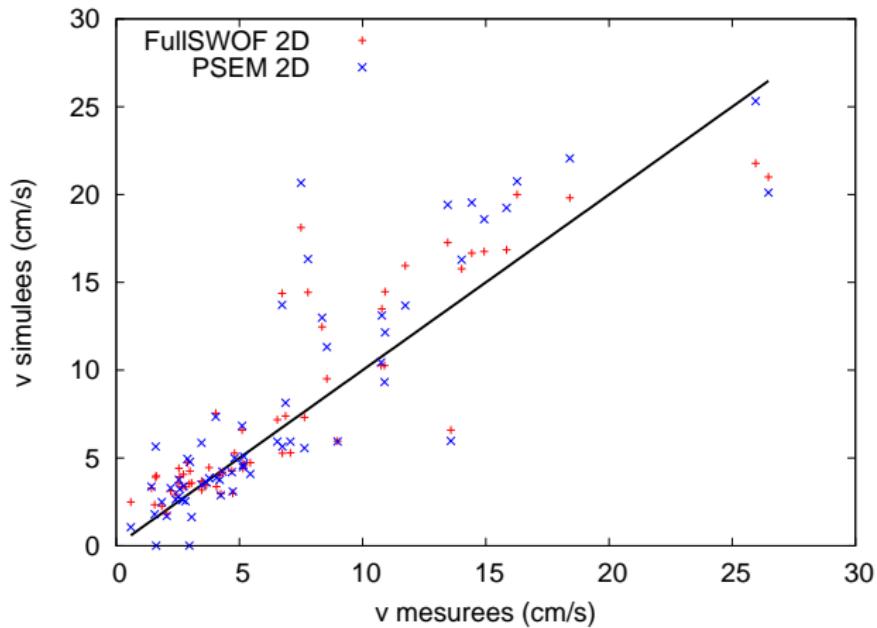
## Heterogeneous coefficients



# Thies parcel – Senegal ([Tatard et al., 2008], IRD)

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## Velocities



## FullSWOF

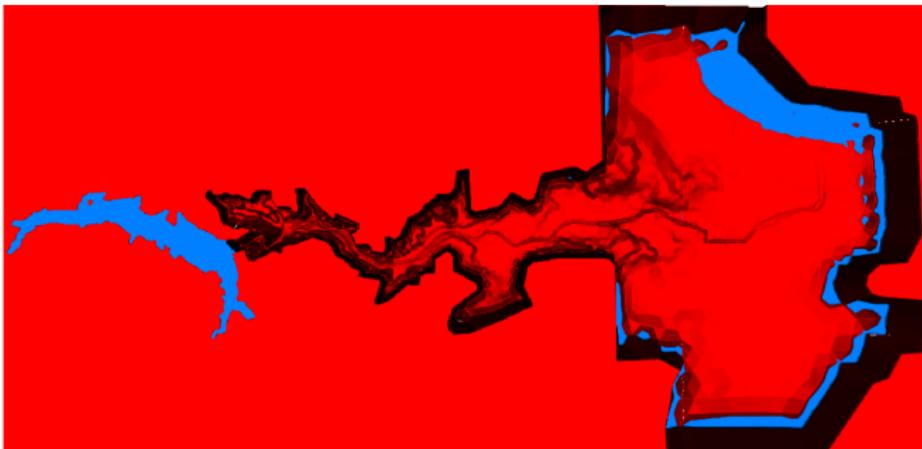
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- ▶ object and inheritance
- ▶ variables encapsulation
- ▶ vector class (2d)
- ▶ objects " distributor"
- ▶ fixed CFL and fixed  $\Delta t$
- ▶ Doxygen documentation
- ▶ Free open source software

# Malpasset dam break simulation

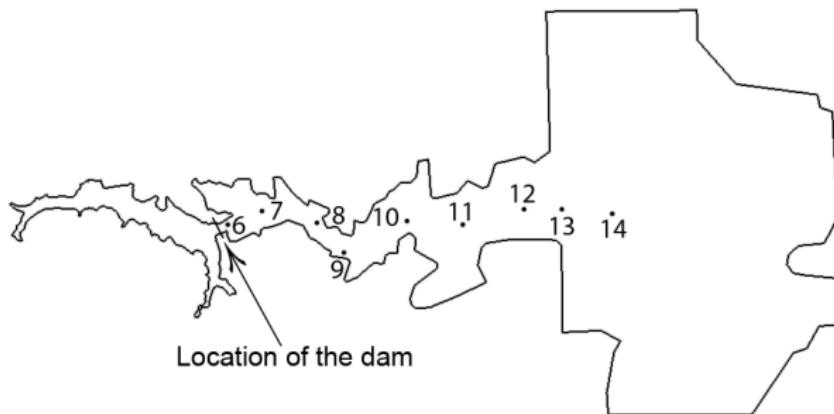
(Cordier et al., CEMRACS 2012)

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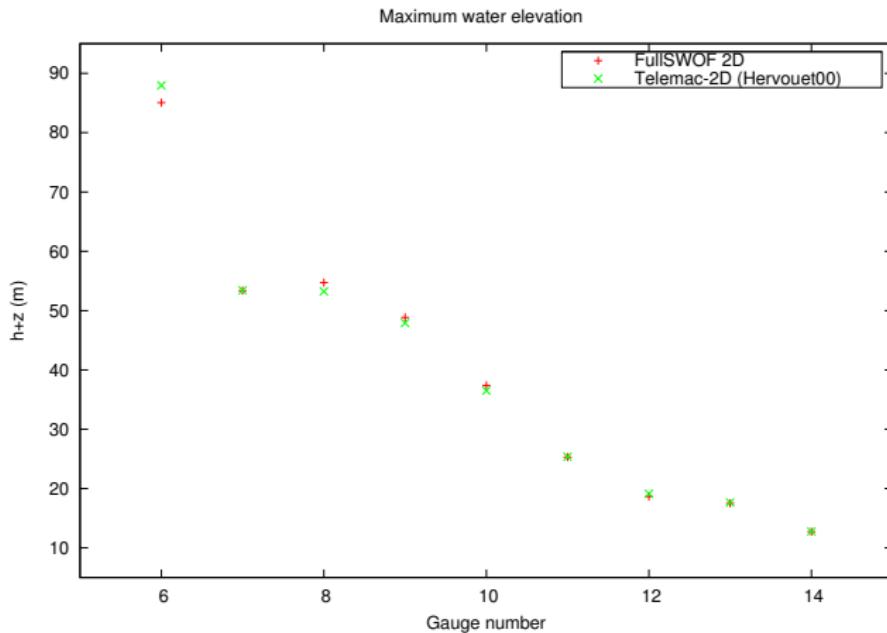
# Malpasset dam break simulation

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# Malpasset dam break simulation

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Thank You !

## HLL flux

$$\mathcal{F}(U_G, U_D) = \begin{cases} F(U_G) & \text{if } 0 < c_1 \\ F(U_D) & \text{if } c_2 < 0 \\ \frac{c_2 F(U_G) - c_1 F(U_D)}{c_2 - c_1} + \frac{c_1 c_2 (U_D - U_G)}{c_2 - c_1} & \text{else} \end{cases},$$

with two parameters

$$c_1 < c_2.$$

For  $c_1$  and  $c_2$ , we take

$$c_1 = \inf_{U=U_G, U_D} \left( \inf_{j \in \{1, 2\}} \lambda_j(U) \right) \text{ and } c_2 = \sup_{U=U_G, U_D} \left( \sup_{i \in \{1, 2\}} \lambda_i(U) \right).$$

with  $\lambda_1(U) = u - \sqrt{gh}$  and  $\lambda_2(U) = u + \sqrt{gh}$ .

▶ retour

-  Audusse, E., Bouchut, F., Bristeau, M.-O., Klein, R., and Perthame, B. (2004).  
A fast and stable well-balanced scheme with hydrostatic reconstruction for shallow water flows.  
SIAM J. Sci. Comput., 25(6) :2050–2065.
-  Bouchut, F. (2004).  
Nonlinear stability of finite volume methods for hyperbolic conservation laws, and well-balanced schemes for sources, volume 2/2004.  
Birkhäuser Basel.
-  Bristeau, M.-O. and Coussin, B. (2001).  
Boundary conditions for the shallow water equations solved by kinetic schemes.  
Technical Report 4282, INRIA.
-  Delestre, O. and Marche, F. (2010).  
A numerical scheme for a viscous shallow water model with friction.  
J. Sci. Comput., DOI 10.1007/s10915-010-9393-y.
-  Esteves, M., Faucher, X., Galle, S., and Vauclin, M. (2000).  
Overland flow and infiltration modelling for small plots during unsteady rain : numerical results versus observed values.  
Journal of Hydrology, 228 :265–282.

 Planchon, O., Silvera, N., Gimenez, R., Favis-Mortlock, D., Wainwright, J., Le Bissonnais, Y., and Govers, G. (2005).  
An automated salt-tracing gauge for flow-velocity measurement.  
Earth Surface Processes and Landforms, 30(7) :833–844.

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